

Effect of fiber type on the bending and uniaxial tensile properties of high-strength high-ductility cementitious composites

Guo Liping^{1,2} Chen Bo³ Wu Yue^{1,2} Lei Dongyi^{1,2}

(¹ School of Materials Science and Engineering, Southeast University, Nanjing 211189, China)

(² Jiangsu Key Laboratory of Construction Materials, Southeast University, Nanjing 211189, China)

(³ State Key Laboratory of Hydrology-Water Resources and Hydraulic Engineering, Nanjing Hydraulic Research Institute, Nanjing 210029, China)

Abstract: To investigate the effect of fiber types on bending and tensile properties of high-strength, high-ductility cementitious composites (HS-HDCCs), ultra-high-molecular-weight polyethylene (PE) fibers, polyvinyl alcohol (PVA) fibers, and copper-plated micro steel fibers were selected as the reinforcement materials. The bending and tensile properties of HS-HDCCs with different fibers with a volume fraction of 2% were studied. The results indicate that PE, PVA, micro steel, and PVA-PE hybrid fibers impart varying degrees of toughening and improve the tensile strength. During the tensile and bending processes, HS-HDCCs with micro steel fibers exhibit a strain-softening phenomenon. HS-HDCCs with PVA fibers or with PVA-PE hybrid fibers can achieve multiple cracking behaviors and strain hardening phenomenon to a certain extent and show slight high-ductility characteristics. HS-HDCCs with PE fibers exhibit multiple cracking behavior and strain hardening phenomenon and show significant high-ductility characteristics. The test results can provide a basis for selecting fibers suitable for HS-HDCCs reinforcement.

Key words: fiber; high ductility; toughness; uniaxial tensile
DOI: 10.3969/j.issn.1003-7985.2018.04.012

High-ductility cementitious composites (HDCCs) are composite materials comprising of a cement-based matrix and short reinforcing fibers. They are highly ductile materials exhibiting multiple fine cracks and pseudo strain-hardening characteristics under uniaxial tensile stresses^[1].

HDCCs have extensive application prospects in seismic strengthening, repairing, and beam and column joint reinforcement of fabricated buildings^[2-3]. Currently, polyvinyl alcohol (PVA) fibers are commonly used to prepare HDCCs having a compressive strength of approximately 60 MPa^[4]. The demand for high-strength (HS)-HDCCs is increasing with the development of prefabricated

buildings. To achieve multiple cracking behavior and high-ductility characteristics, the energy and strength criteria need to be met. This requires the congruence of matrix materials and fiber properties^[5]. A challenging aspect of research on HS-HDCCs materials is coordinating the fiber and matrix properties to achieve high ductility with a matrix strength of over 100 MPa.

This study aims to investigate the influence of fiber types, i.e., polyethylene (PE), PVA, and copper-plated micro steel fibers, on HS-HDCCs' bending toughness and tensile properties. Also, the effect of PVA-PE hybrid fibers on HS-HDCCs' performance is tested in experiments.

1 Experiment

1.1 Materials

The cement used in the HS-HDCCs mixtures is P · I 52.5 Portland cement. Its physical properties and chemical composition are listed in Tab. 1 and Tab. 2, respectively. The silica fume, with its chemical composition listed in Tab. 2, has a silicon dioxide content of 95.2%, a loss of 1.04% on ignition, a density of 2 500 kg/m³, and a specific surface area of 22 000 m²/kg. The aggregate used is sieved river sand with a maximum grain size of 0.60 mm. A polycarboxylate-type high-performance water-reducing agent with a solid content of 40% is used along with ordinary tap water.

Tab. 1 Physical and mechanical properties of cement

| Water requirement of normal consistency/% | Setting time/min | | Flexural strength/MPa | | Compressive strength/MPa | |
|---|------------------|---------------|-----------------------|------|--------------------------|------|
| | Initial setting | Final setting | 3 d | 28 d | 3 d | 28 d |
| 26.3 | 140 | 362 | 7.2 | 10.6 | 34.7 | 62.8 |

PE, PVA, and copper-plated micro steel fibers are used herein. The physical and mechanical properties of the fibers are listed in Tab. 3.

1.2 HS-HDCCs mixing proportion and specimen preparation

The mix proportion parameters of HS-HDCCs are shown as follows: The water-to-binder ratio is 0.23, the silica fume replacement is 30%, the dosage of the water-reducing agent is 2%, and the fine aggregate-to-binder ratio is 0.36.

Received 2018-02-01, Revised 2018-06-10.

Biography: Guo Liping (1979—), female, doctor, associate professor, guoliping691@163.com.

Foundation items: The National Key Research and Development Program of China (No. 2016YFC0401610), the National Natural Science Foundation of China (No. 51778133, 51739008, 51438003).

Citation: Guo Liping, Chen Bo, Wu Yue, et al. Effect of fiber type on the bending and uniaxial tensile properties of high-strength high-ductility cementitious composites [J]. Journal of Southeast University (English Edition), 2018, 34(4): 495 – 499. DOI: 10.3969/j.issn.1003-7985.2018.04.012.

Tab. 2 Chemical composition of cement and silica fume

| Binder | w(CaO) | w(SiO ₂) | w(Al ₂ O ₃) | w(Fe ₂ O ₃) | w(MgO) | w(SO ₃) | w(Other) |
|-------------|--------|----------------------|------------------------------------|------------------------------------|--------|---------------------|----------|
| Cement | 64.70 | 20.40 | 4.70 | 3.38 | 0.87 | 1.88 | 4.06 |
| Silica fume | 0.014 | 95.2 | 0.913 | 1.445 | 0.382 | 0 | 2.046 |

Tab. 3 Physical and mechanical properties of fibers

| Fiber type | Equivalent diameter/ μm | Elastic modulus/GPa | Ultimate tensile strength/MPa | Ultimate elongation/% | Length/mm | Density/($\text{g} \cdot \text{cm}^{-3}$) |
|-------------------|------------------------------------|---------------------|-------------------------------|-----------------------|-----------|---|
| PE fiber | 24 | 116 | 2 100 | 8 to 10 | 12 | 0.97 |
| PVA fiber | 40 | 35 | 1 350 | 6 to 8 | 12 | 1.3 |
| Micro steel fiber | 200 | 200 | 2 850 | 3 to 4 | 13 | 7.8 |

The fiber volume fraction is maintained throughout as 2%. The fiber volume fractions of HS-HDCCs are shown in Tab. 4.

Tab. 4 The fiber volume fraction of HS-HDCCs

| Mixture | PE fiber | PVA fiber | Micro steel fiber |
|----------|----------|-----------|-------------------|
| PE2 | 2 | 0 | 0 |
| PVA2 | 0 | 2 | 0 |
| ST2 | 0 | 0 | 2 |
| PVA1-PE1 | 1 | 1 | 0 |

The HS-HDCC specimen preparation process is as follows:

- 1) Cement, silica fume, and sand are mixed for 2 min.
- 2) Water and water-reducing agent are mixed with the above-mentioned mixture for 2 to 3 min to prepare a uniform paste.
- 3) The fibers are then evenly fed into a mixer within 1 min.
- 4) Subsequently, the mixture is then homogenized for another 5 min.
- 5) Next, the mixture is poured into a vibrating mold with two layers, and its top surface is covered with plastic sheeting.
- 6) Finally, the mold is removed after 24 h and the specimen is placed into a curing box at a temperature of $(20 \pm 3)^\circ\text{C}$ and a relative humidity of $\geq 95\%$.

1.3 Test methods

Flexural and compressive strength tests: The mechanical properties were measured by using prism specimens with a dimension of 40 mm \times 40 mm \times 160 mm at the age of 28 d according to the method of testing cements-determination of strength (ISO) (GB/T 17671—1999).

Bending toughness tests: According to the standard test methods for fiber-reinforced concrete (CECS13:2009), a four-point bending test was conducted by using thin-plate specimens with a dimension of 300 mm \times 75 mm \times 15 mm the at age of 28 d. Bending tests were conducted by using an MTS 810 servo-hydraulic testing system in the displacement-control mode with a loading rate of 0.5 mm/min. Complete bending stress-mid-span deflection curves were recorded.

Uniaxial tensile tests: The tensile properties were evaluated according to the Japan Society of Civil Engineers' code *Recommendations for Design and Construction of*

High Performance Fiber Reinforced Cement Composites with Multiple Fine Cracks. The dumbbell-shaped specimens with a thickness of 13 mm, parallel portion width of 30 mm, parallel portion length of 100 mm, and original reference point distance of 100 mm were used. Uniaxial tensile tests were conducted by using the MTS 810 servo-hydraulic testing system in displacement-control mode at a loading rate of 0.3 mm/min. Aluminum plates were glued on both sides of the dumbbell-shaped specimens to facilitate gripping. Two external linear-variable displacement transducers with a gauge length of about 100 mm were attached to the specimens in order to measure the elongation of the specimens. Complete tensile stress-strain curves were recorded. Herein, the ultimate tensile strain of each HDCCs specimen is defined as the strain at the softening point of the uniaxial tensile stress-strain curves, whereas the ultimate tensile stress is defined as the value of the maximum stress obtained in the strain-hardening region.

2 Results and Discussion

2.1 Flexural and compressive strengths of HS-HDCCs

The results of the flexural and compressive strength tests of four HS-HDCCs are presented in Fig. 1 and Fig. 2.

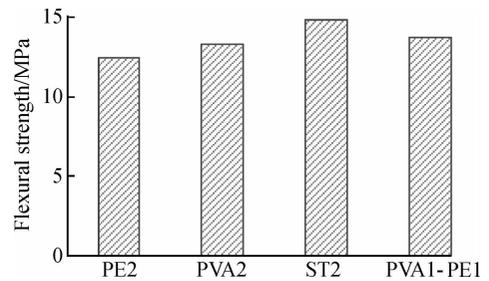


Fig. 1 Flexural strength of HS-HDCCs

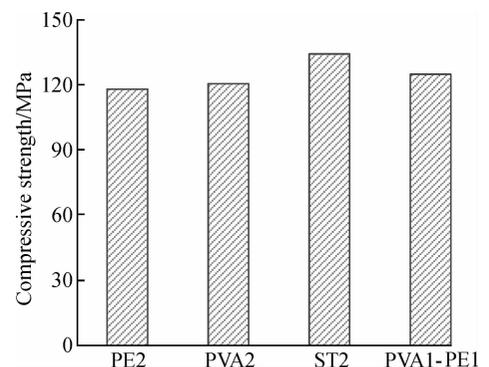


Fig. 2 Compressive strength of HS-HDCCs

With a water-to-binder ratio of 0.23 and a silica fume replacement level of 30%, the flexural and compressive strengths of the four HS-HDCCs were in the ranges of 12.4 to 14.8 MPa and 118.1 to 134.2 MPa, respectively. HS-HDCCs with PE fibers and those with PVA fibers exhibited similar mechanical properties. HS-HDCCs with PVA-PE hybrid fibers exhibited greater strength compared with the HS-HDCCs reinforced with either PE or PVA fibers. The fiber hybrid effect improves the mechanical properties of HDCCs. Micro steel fibers were found to remarkably improve the mechanical properties. In comparison with PE2, the ST2 specimen's flexural strength and compressive strength increased by approximately 20% and 15%, respectively. Compared with organic synthetic fibers, the effect of micro steel fiber on improving the mechanical properties of concrete is more obvious.

2.2 Bending toughness of HS-HDCCs

The bending stress-mid-span deflection curves of the four groups of HS-HDCCs are presented in Fig. 3. The bending strength of PE2, PVA2, ST2, and PVA1-PE1 are 7.3, 10.5, 29.4, and 13.8 MPa, respectively. The corresponding values of mid-span deflection curves, also known as the absorbed energy, are 7 781, 1 980, 8 501, and 6 392 N · mm, respectively. As shown in Fig. 3, ST2 has the highest bending strength and energy absorption capacity, indicating that the micro steel fibers have significant toughening effects. It can also be observed that the deflection of ST2 is small and that the load-carrying capacity rapidly decreases beyond the peak point. This is the typical strain-softening behavior, which shows no multiple cracking characteristics. PE2 has the lowest bending strength and the highest mid-span deflection. The multiple cracking characteristics are obvious during bending (see Fig. 4), and the energy absorption capacity is at an upper-middle level. Although the bending strength of PVA2 is higher than that of PE2, the toughening effect of PVA fibers is not significant and the strain-hardening characteristics are not prominent. The energy absorption capacity and mid-span deflection of the PVA1-PE1 group are between the PVA2 and PE2 values. The hybrid PVA-PE fibers improve the bending strength. The bending stress-mid-span deflection curve is clearly serrated and has multiple cracking characteristics, indicating a strain-hardening failure mode. The hybrid fibers have a superior toughening effect compared with PVA fibers.

In summary, PE, PVA, micro steel fibers and hybrid PVA-PE fibers have a toughening effect on HS-HDCCs, as shown in the bending toughness tests. HS-HDCCs reinforced with micro steel fibers show no obvious multiple cracking characteristics or the strain-softening failure. HS-HDCCs with PVA fibers exhibit slight strain-hardening characteristics, whereas HS-HDCCs with PE fibers or hybrid PVA-PE fibers exhibit clear multiple cracking

characteristics and strain-hardening failure.

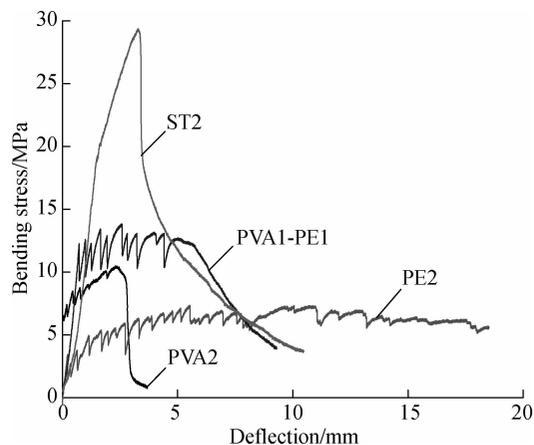


Fig. 3 A plot of bending stress vs. mid-span curve of HS-HDCCs



Fig. 4 Multiple cracks of bending HS-HDCCs specimens with PE fibers

2.3 Uniaxial tensile properties of HS-HDCCs

The uniaxial tensile test results of HS-HDCCs are shown in Fig. 5. The initial crack strengths of PE2, PVA2, ST2, and PVA1-PE1 are 3.2, 3.5, 6.4, and 4.4 MPa, respectively. PE, PVA, and micro steel fibers as well as hybrid PVA-PE fibers were all found to increase the tensile strengths of HS-HDCCs. The ultimate tensile strengths of PE2, PVA2, ST2, and PVA1-PE1 are 4.7, 6.0, 8.2, and 5.9 MPa, respectively, whereas the ultimate tensile strains are 3.15%, 0.62%, 0.80%, and 0.90%, respectively. As shown in Fig. 4, although ST2 has the highest tensile strength, it only develops one crack during the tensile process and does not show high-ductility characteristics. The tensile strengths and ultimate tensile strains of PVA2 and PVA1-PE1 are similar wherein the tensile strain is less than 1% and the strain-hardening and multiple cracking phenomena are observed; however, their characteristics are not significant. The hybrid PVA-PE fibers exhibit enhanced strain-hardening effects.

PE2 has the lowest tensile strength; however, its strain-hardening and multiple cracking characteristics are rather significant (see Fig. 6). Additionally, it can be classified as a high-ductility material.

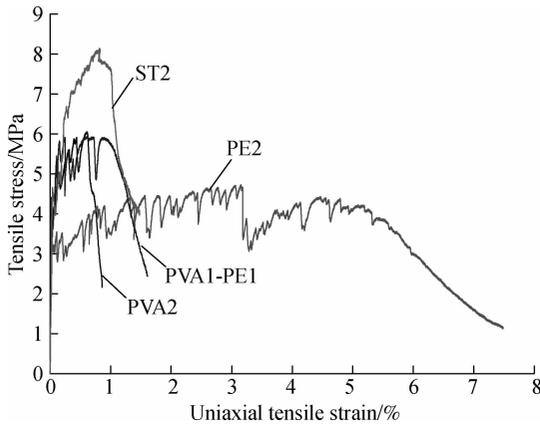


Fig. 5 A plot of uniaxial tensile stress vs. strain curve of HS-HDCCs

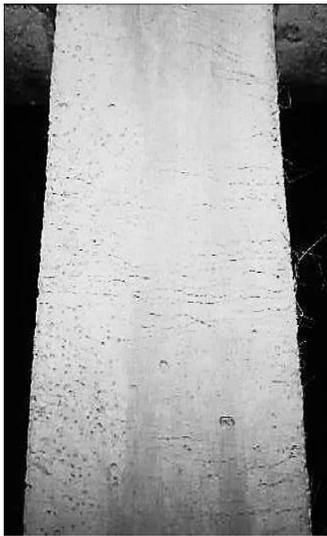


Fig. 6 Multiple cracks of uniaxial tensile HS-HDCCs with PE fibers

In summary, PE, PVA, and micro steel fibers as well as hybrid PVA-PE fibers were found to improve the tensile strength of HS-HDCCs in the uniaxial tensile test. The micro steel fibers only increased the tensile strength of HS-HDCCs and did not exhibit high ductility. In contrast, the PVA fibers and hybrid PVA-PE fibers exhibited high ductility; however, the effect was not obvious. Furthermore, PE fibers were found to exhibit significantly high ductility.

A comprehensive analysis of Fig. 3 and Fig. 5 indicates that the bending stress-mid-span deflection curves of the HS-HDCCs were similar to the uniaxial tensile stress-strain curves. This is mainly related to the physical and mechanical properties of the fibers.

The micro steel fibers have high tensile strength and strong matrix adhesion that can significantly increase the toughness of the matrix. However, once debonding oc-

curs between steel fibers and the matrix, the friction between them sharply decreases and the slip-hardening coefficient value becomes less than zero. Therefore, steel fibers exhibit strain softening behavior during bending and uniaxial tensile tests^[6].

As PVA fibers have hydrophilic surfaces, they exhibit high adhesive strengths when a low water-to-binder ratio and high-strength matrix are used. Additionally, PVA fibers have certain toughening effects and can cause high frictional bonding that can ultimately fracture the fiber and reduce the energy absorption capacity during the bending or tensile process^[7-8].

PE fiber surfaces are hydrophobic; therefore, the adhesive forces between PE and the matrix are relatively low. Moreover, PE fibers have considerably high tensile strength that causes them to be pulled out rather than be fractured during tension. They continue to bear the tensile load after debonding, and the slip-hardening coefficient is greater than zero^[9-10]. Consequently, PE2 exhibits strain-hardening characteristics. In comparison with the PVA and micro steel fibers, the diameters of the PE fibers used are smaller. If there are more fibers with the same fiber volume fraction, the strain-hardening phenomenon will be more significant.

3 Conclusions

1) PVA, PE, and PVA-PE hybrid fibers have little effect on the flexural and compressive strengths of HS-HDCCs. The micro steel fibers can improve the mechanical properties of HS-HDCCs in the range of 15% to 20%.

2) PE, PVA, and micro steel fibers as well as hybrid PVA-PE fibers, all have a toughening effect and can increase the tensile strength of HS-HDCCs.

3) During the tensile and bending processes, HS-HDCCs with micro steel fibers exhibit the strain-softening phenomenon. The HS-HDCCs with PVA fibers and those with hybrid PVA-PE fibers achieve multiple cracking behavior and strain hardening phenomenon to a certain extent and exhibit slightly high ductile characteristics. The HS-HDCCs with PE fibers achieve remarkable multiple cracking behavior and strain-hardening phenomena and exhibit significant high-ductility characteristics.

References

- [1] Li V C. Progress and application of engineered cementitious composites[J]. *Journal of the Chinese Ceramic Society*, 2007, **35** (4): 531 – 536. DOI: 10. 3321/j. issn: 0454-5648. 2007. 04. 026. (in Chinese)
- [2] Guo L P, Chen B, Sun W, et al. Effect of expansive agent on mechanical properties and deformation behavior of high ductility cementitious composites[J]. *Journal of the Chinese Ceramic Society*, 2016, **44** (11): 1609 – 1613. DOI:10. 14062/j. issn. 0454-5648. 2016. 11. 10. (in Chinese)
- [3] Guler M, Jashami H, Yaman I O, et al. Thin ECC over-

- lay systems for rehabilitation of rigid concrete pavements [J]. *Magazine of Concrete Research*, 2013, **65**(2):108 - 120. DOI:10.1680/mac.12.00022.
- [4] Guo L P, Zhu C G, Fan Y G, et al. Design and application of high ductility cementitious composites for bridge deck link slab repair [J]. *China Concrete and Cement Products*, 2016(12):36 - 39. (in Chinese)
- [5] Pang C M, Leung Christopher K Y, Sun W. Review on preparation technology of high ductility cementitious composites [J]. *Journal of Hebei University of Technology*, 2014, **43**(6):17 - 21. (in Chinese)
- [6] Lee Y, Kang S T, Kim J K. Pullout behavior of inclined steel fiber in an ultra-high strength cementitious matrix [J]. *Construction and Building Materials*, 2010, **24**(10):2030 - 2041. DOI:10.1016/j.conbuildmat.2010.03.009.
- [7] Zhang J, Wang Q, Wang Z B. Properties of polyvinyl alcohol-steel hybrid fiber reinforced composite with high-strength cement matrix [J]. *Journal of Materials in Civil Engineering*, 2017, **29**(7): 04017026. DOI:10.1061/(asce)mt.1943-5533.0001868.
- [8] Li V C. Interface tailoring for strain-hardening PVA-ECC [J]. *ACI Materials Journal*, 2002, **99**(5): 463 - 472.
- [9] Choi J I, Song K I, Song J K, et al. Composite properties of high-strength polyethylene fiber-reinforced cement and cementless composites [J]. *Composite Structures*, 2016, **138**:116 - 121. DOI: 10.1016/j.compstruct.2015.11.046.
- [10] Guo L P, Chen B, Sun W, et al. Effects of aggregate type and fibre on properties of high ductility cementitious composites [J]. *Journal of Southeast University (Natural Science Edition)*, 2017, **47**(6):1221 - 1226. (in Chinese)

纤维类型对高强高延性水泥基复合材料弯拉性能的影响

郭丽萍^{1,2} 陈波³ 吴樾^{1,2} 雷东移^{1,2}

(¹ 东南大学材料科学与工程学院, 南京 211189)

(² 东南大学江苏省土木工程材料重点实验室, 南京 211189)

(³ 南京水利科学研究院水文水资源与水利工程科学国家重点实验室, 南京 210029)

摘要:为了考察纤维类型对高强高延性水泥基复合材料(HS-HDCC)弯曲与拉伸性能的影响,选取了超高分子量聚乙烯(PE)纤维、聚乙烯醇(PVA)纤维和镀铜微细钢纤维3种纤维在体积掺量为2%时,研究不同类型纤维对HS-HDCC的弯曲与拉伸性能的影响.结果表明:PE,PVA和微细钢纤维单掺或PVA-PE混杂,均对HS-HDCC有增韧和提高抗拉强度的效果.在弯曲和拉伸过程中,HS-HDCC单掺微细钢纤维时呈应变软化破坏;单掺PVA纤维和PVA-PE混杂可在一定程度上实现多缝开裂和应变硬化,有一定的高延性特性;单掺PE纤维可明显实现多缝开裂和应变硬化,有显著的高延性特性.研究结果为HS-HDCC优选合适的纤维提供了依据.

关键词:纤维;高延性;弯曲韧性;单轴拉伸

中图分类号:TU528